



# **LUXEON Altilon SMD DT**

Assembly and Handling Information



## Introduction

This application brief addresses the recommended assembly and handling procedures for LUXEON Altilon SMD DT. LUXEON Altilon SMD DT is designed to deliver daytime running light and turn indicator within one LED. This is enabled by combining with one white emitter and one phosphor converted amber emitter in one package.

Due to the small size and construction, they require special assembly and handling precautions. Proper assembly, handling and thermal management, as outlined in this application brief, ensures high optical output, long term lumen maintenance and high reliability of LUXEON Altilon SMD DT in automotive applications.

## Scope

The assembly and handling guidelines in this application brief apply to the following product(s):

#### **PRODUCTS**

LUXEON Altilon SMD DT

Any assembly or handling requirements that are specific to a subset of LUXEON Altilon SMD DT products is clearly marked.

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## 1. Component

#### 1.1 Reference Document

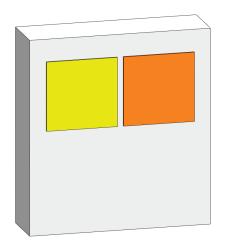
The LUXEON Altilon SMD DT datasheet DS233 is available on request. Please contact your sales representative.

### 1.2 Description

The LUXEON Altilon SMD DT consists of an array of two LED chips combined with one phosphor converter to emit white light and one phosphor converter to emit amber light. They are mounted onto a ceramic substrate. Underneath the substrate are electrical pads. An electrical interconnect layer connects the LED chips to a cathode and anode on the bottom of the ceramic substrate.

Combining the two light emitting phosphor converters in one LED it is possible to achieve a closer distance of the emitting areas as it would be possible with two separate LED.

The outside of the package is coated with white silicone to shield the chip from the environment. and It also prevents light leakage to the sides and optical crosstalk between the two individually operated phosphor converters. The LUXEON Altilon SMD DT includes two separate transient voltage suppressor (TVS) chips on top of the carrier substrate.



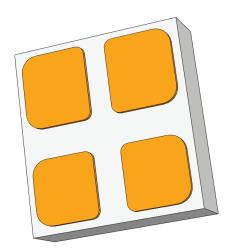


Figure 1. Top view (left) and bottom view (right) of the LUXEON Altilon SMD DT

Table 1. Design features of Altilon SMD DT

PRODUCT	PART NUMBER	NOMINAL DRIVE CURRENT	DIE SIZE	LIGHT EMITTING AREA	PACKAGE SIZE
LUXEON Altilon SMD DT	A1SB – DT012DH0xxxxx	1000 mA /1000 mA	1 mm²	1.06 mm x 1.06 mm	2.7 mm x 3 mm

#### 1.3 Form Factor

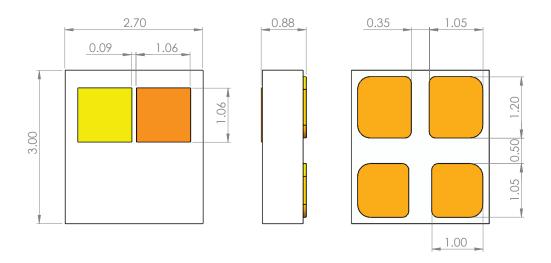


Figure 2. Dimensions in milimeters for Altilon SMD DT

## 1.4 Optical Crosstalk

Optical crosstalk in the Altilon SMD DT is the effect that the operated LED stimulates the 2<sup>nd</sup> phosphor converter which then emits light of a different color. There are two kinds of crosstalk:

- 1. Only the white LED is operated and the amber phosphor converter also emits light.
- 2. Only the amber LED is operated and the white phosphor converter also emits light.

Typical measured values are <1 %.

For detailed information please contact your sales representative.

#### 1.5 Mechanical Files

Mechanical drawings for LUXEON Altilon SMD DT (2D and 3D) are available upon request. For details, please contact your sales representative.

## 2. Handling Precautions

Like all electrical components, there are handling precautions that need to be taken into account when setting up assembly procedures. The precautions for LUXEON Altilon SMD DT are noted in this section.

## 2.1 Electrostatic Discharge (ESD) Protection

Electrostatic discharge, rapid transfer of charges between two bodies due to an electrical potential difference between those bodies, can cause damage to electronic components. In LED devices, ESD events can result in a slow degradation of light output and/or early catastrophic failures. In order to prevent ESD from causing any damage, Lumileds devices include a protection diode that is in parallel to the chip. This transient voltage suppressor (TVS) diode provides a current path for transient voltages (see Figure 3).

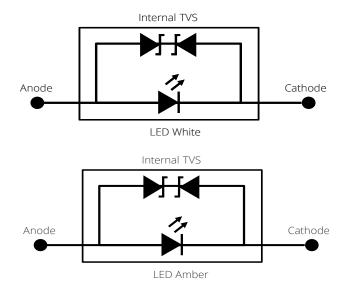


Figure 3. Electrical schematic of a Lumileds LED with bi-directional TVS for LUXEON Altilon SMD DT

Common causes of ESD include the direct transfer of charges from the human body or from a charged conductive object to the LED component. In order to test the susceptibility of LEDs to these common causes of ESDs, three different models are typically used:

- Human Body Model (HBM)
- · Machine Model (MM)
- · Charged Device Model (CDM)

LUXEON Altilon SMD DT emitters have been independently verified to successfully pass ESD tests under HBM, MM and CDM conditions. For the respective test voltages of these tests please refer to the latest LUXEON Altilon SMD DT datasheets. Nevertheless, Lumileds strongly recommends that customers adopt handling precautions for LEDs similar to those which are commonly used for other electronic surface mount components which are susceptible to ESD events. Additional external ESD protection for the LED may be needed if the LED is used in non ESD-protected environments and/ or exposed to higher ESD voltages and discharge energies, e.g. as described in ISO 10605 or IEC 61000-4-2 (severity level IV). For details please contact your sales representative.

### 2.2 Component Handling

Minimize all mechanical forces exerted onto the LED package. The white package consists of fragile silicone material and should not be handled with tweezers that can lead to damage of the package, especially not with metallic tweezers. Any force above 2.0N may damage the silicone side coat and change optical performance. A vacuum pen can be used instead of tweezers (see Figure 4).

The suction tip should be made of a soft material such as rubber to minimize the mechanical force exerted onto the top surface of the LED and apply no forces to the silicone side coat layer. Avoid contaminating the top side surface of the LED with the soft material. Do not stick any tape on top of the light emitting surface, such as capton- or UV-tape. A contamination of glue or its invisible constituent parts may change the LED performance.

Electrical testing before assembly should be avoided. Probe tips may scratch or dent the pad surface, which may lead to solder issues, and damage the LED. Avoid contact with the LED other than what is required for placement.







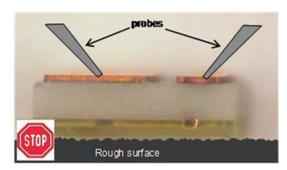
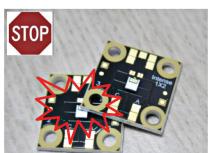


Figure 4. LED handling for LUXEON Altilon SMD DT

Do not touch the top surface with fingers or apply any pressure to it when handling finished boards containing LUXEON Altilon SMD DT emitters. Do not stack finished boards because the LED can be damaged by the other board outlines. In addition, do not put finished boards with LUXEON Altilon SMD DT emitters top side down on any surface. The surface of a workstation may be rough or contaminated and may damage the LED. These warnings are shown in Figure 5.





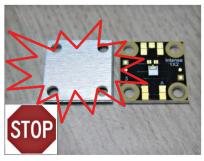


Figure 5. Board handling for LUXEON Altilon SMD DT

In order to avoid any electrical shocks and/or damage to the LEDs, each design needs to comply with the appropriate standards of safety and isolation distances, known as clearance and creepage distances, respectively (e.g. IEC60950, clause 2.10.4).

## 2.3 Cleaning

The surface of the LED should not be exposed to dust and debris. Excessive dust and debris on the LED surface may cause a decrease in light output and optical behavior. It is best to keep LEDs in their original shipping reel until actual use.

In the event that the surface requires cleaning, a compressed gas duster or an air gun with 1.4 bar (at the nozzle tip), a distance of 15 cm will be sufficient to remove the dust and debris. Make sure the parts are secured first, taking above handling precautions into account.

One can also rinse with isopropyl alcohol (IPA). Do not use solvents that are listed in Table 13, as they may adversely react with the LED assembly. Extra care should be taken not to damage the housing around the LED chips. Lumileds does not recommend ultrasonic supported cleaning for LUXEON Altilon SMD DT emitters.

## 3. Printed Circuit Board

### 3.1 PCB Requirements

The LUXEON Altilon SMD DT can be mounted on multi-layer FR4 printed circuit boards (PCB) or insulated metal substrates (IMS). To ensure optimal operation of the LED, the thermal path between the LED package and the heat sink should be optimized according to the application requirements. Please ensure that the PCB assembly complies to the applicable IPC standards listed below.

#### **General PCB Standards:**

- IPC A-600J: Acceptability of Printed Boards
- IPC A-610G: Acceptability of Electronic Assemblies
- IPC 2221B: General Standard on Printed Board Design
- IPC 7093: Design and Assembly Process Implementation for Bottom Termination Components

#### Filled and capped via boards:

- IPC 4761: Design Guide for Protection of Printed Board Via Structures
- IPC 2315: Design Guide for High Density Interconnects and Micro Vias
- IPC 2226A: Design Standard for High Density Interconnect Printed Boards

## 3.2 Footprint and Land Pattern

Lumileds recommends using solder mask defined land pattern for LUXEON Altilon SMD DT, as shown in Figure 6. Due to this, the copper area can be extended as far as possible for better heat spreading, which results in lower thermal resistance. However, a solder mask defined pad requires good mask quality and tight registration tolerances during PCB manufacturing (see section 3.6 "PCB Quality and Supplier" for more details).

For the solder mask defined land pattern, the self-alignment of the component during reflow soldering can be controlled well by solder mask geometry in X- and Y-direction.

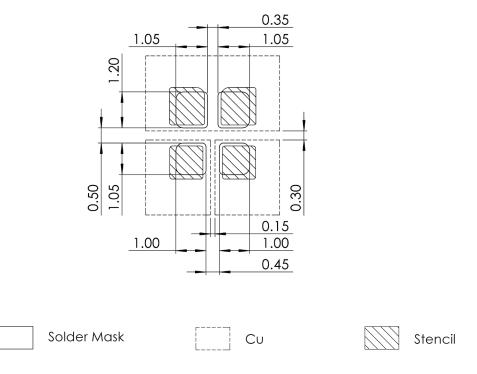


Figure 6. Solder mask defined land pattern for LUXEON Altilon SMD DT

The metal-defined land pattern leaves less area for heat spreading of the thermal power generated by the LED. Also, higher tolerances for LED tilting and position tolerances can be encountered. The positive aspect is that the requirements to the printed circuit board tolerance requirements for solder mask alignment to metal structure are lower than for solder mask defined land pattern.

### 3.3 Surface Finishing

Lumileds recommends using ENIG (Electroless Nickel Immersion Gold) plating according to IPC-4552. Other surface finishes are possible but have not been tested by Lumileds. Surface finish Hot-Air-Solder-Leveling (HASL) may lead to inhomogenious pad height and is not recommended. Unsymmetrical solder thickness may have an influence on LED height and soldering tolerances. The actual quality of HASL finish shall be checked in each single case.

#### 3.4 Solder Mask

A flat solder mask thickness on top of metal layer is desired. Solder mask thickness variation and offset tolerances have impact on solder quality and post-solder position accuracy. Mask and PCB vendors have to be evaluated for proper quality. Detailed specifications and information regarding solder mask requirements are contained in IPC-6012 and IPC-SM-840. (see Chapter 3.6 Figure 7 for more details).

## 3.5 Silk Screen or Ink Printing

Silk screen markings within and around the LED outline should be avoided because the height of the ink may interfere with solder stencil printing process.

## 3.6 PCB Quality and Supplier

Select only PCB suppliers that are capable of delivering the required level of quality. Leastwise, the PCBs must comply with IPC standard IPC-A-600J, 2016 ("Acceptability of Printed Boards").

A maximum mask registration tolerance of 50  $\mu$ m between the copper trace pattern and solder mask is desirable to achieve optimum solder joint contact area. If the offset between the solder mask and the copper land pattern is large, one side of electrode pads will have less solder joint contact area. This may affect package centering, tilting, and thermal performance and may increase risk of solder bridging (short circuit) and solder balling if the stencil is not properly aligned to the solder mask during printing.

Figure 7 shows an example of the solder pad size for three different registration offset levels between the copper trace pattern and the solder mask on the PCB. Large misalignment between solder mask opening and copper trace will cause one of the two electrode copper land patterns to be smaller than the other. Depending on the PCB manufacturer capability, PCB cost consideration and customer position tolerance needs, it may be necessary to extend the area of the solder mask opening.

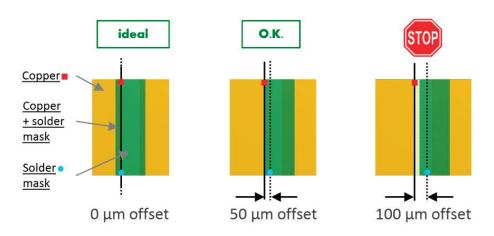


Figure 7. Solder mask registration offset to copper trace for LUXEON Altilon SMD DT

## 4. Thermal Management

#### 4.1 Thermal Resistance

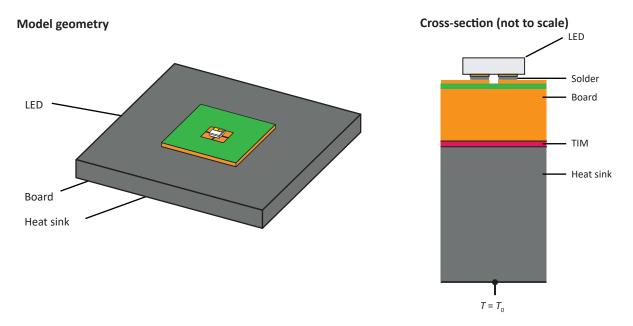
The thermal resistance between the junction of the LED and the bottom side of the PCB depends on the following key design parameters of a PCB:

- · PCB dielectic materials
- · Cu plating thickness
- · Solder pad pattern and solder thickness
- Distance to neighboring heat source (LED spacing)

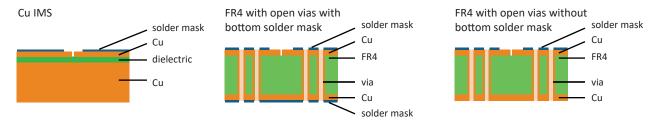
Lumileds conducted simulations to evaluate the thermal performance of LUXEON Altilon SMD DT on different PCB design concepts. Details of the simulation model are given in Figure 8. The model geometry comprises the LUXEON Altilon SMD DT on a board (Cu-IMS board or FR4 board open vias, board area of 20 mm x 20 mm) that is mounted on a plate Al heat sink (dimension of 50 mm x 50 mm x 5 mm). A thermal interface material (TIM) is assumed between board and heatsink. In the simulations, a constant temperature boundary condition ( $T = T_0 = 25$  °C) is imposed at the bottom of the heat sink. More details on the simulation gemeometry and the used material parameters can be found in Table 2. In the simulations, it has been assumed that either the white emitter or the amber emitter is operated.

Table 2 Layer thicknesses and thermal conductivities used in the simulations

Component/Material	Thickness	Thermal conductivity
Al heat sink	10 mm	150 W/(mK)
TIM	100 μm	1 W/(mK)
Board Cu core	1.0 mm	390 W/(mK)
Board FR4	1.5 mm	0.3 W/(mK)
IMS dielectric	38 µm	3 W/(mK)
Top Cu layer	35 μm	390 W/(mK)
Bottom Cu layer (FR4 board)	35 µm	390 W/(mK)
Solder mask	20 μm	0.2 W/(mK)
Vias plating	n.a.	390 W/(mK)
Solder	150 μm	56 W/(mK)



#### **Board cross-sections (not to scale)**



#### Top-side Cu pattern and vias layout

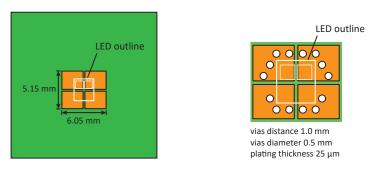


Figure 8. Model geometry and board parameters used for simulations for LUXEON Altilon SMD DT LEDs

The thermal resistance junction-to-board bottom based on eletrical input power  $R_{\text{th,j-b,el}}$  (thermal resistance based on electrical input power) can be calculated as  $R_{\text{th,j-b,el}} = R_{\text{th,j-b,real}}^*$  (1–WPE), where  $R_{\text{th,j-b,real}}$  denotes the thermal resistance based on thermal power and WPE denotes the wall plug efficiency. The WPE is not constant and depends on drive condition and flux binning class. The thermal resistance  $R_{\text{th,j-b,real}}$  is obtained by  $R_{\text{th,j-b,real}} = (T_j - T_b)/P_{\text{th}}$ . Here,  $T_j$  and  $T_b$  denote the junction temperature and the maximum temperature at the bottom side of the board, respectively, obtained from the simulations, and  $P_{\text{th}}$  is the thermal input power. Table 3 lists the simulated thermal resistances  $R_{\text{th,j-b,el}}$  for LUXEON Altilon SMD DT on different board types. To calculate  $R_{\text{th,j-b,el}}$ , a wall-plug efficiency of 0.30 and 0.25 has been used for the CW emitter and the PCA emitter, respectively. Lumileds' recommendation to optimize the thermal performance of the system is to use Cu-based metal-core board with a thermally well performing dielectric.

Table 3. Simulated LED-junction-to-board-bottom thermal resistances  $R_{\text{th,j-b,real}}$  and  $R_{\text{th,j-b,el}}$  for different board types. The thermal resistances  $R_{\text{th,i-b,el}}$  have been calculated assuming a WPE of 0.30 and 0.25 for the CW emitter and the PCA emitter, respectively.

DOADD MATERIAL AND DISLECTIVE	CW		PCA	
BOARD MATERIAL AND DIELECTRIC	R <sub>th,j-b,real</sub> (K/W)	$R_{\rm th,j-b,el}$ (K/W)	R <sub>th,j-b,real</sub> (K/W)	$R_{\rm th,j-b,el}$ (K/W)
1.0 mm Cu-IMS, 3 W/(mK) - 38 μm dielectric	7.2	5.0	7.2	5.4
1.5 mm FR4 with open vias, no bottom solder mask	16.0	11.2	16.0	12.0
1.5 mm FR4 with open vias bottom solder mask	18.8	13.1	18.8	14.2

## 4.2 Close-Proximity Thermal Performance

For small distances between individual LEDs, thermal crosstalk can occur, leading to enhanced junction temperatures. Lumileds recommends using thermally well performing boards with high-conductivity dielectric to optimize the thermal performance. Lumileds conducted thermal simulations of a 2x2 LED arrangement of a board on a heat sink as shown in Figure 9. The board used in the simulations was a Cu-IMS board with the same layer thicknesses and material parameters as outlined in Section 4.1. TIM parameters and heat sink parameters were the same as for the single-LED case described in Section 4.1.

Two different operation modes have been considered: In the first scenario, only the white LEDs are operated, and in the second scenario, only the amber LEDs are operated. In both scenarios, the same power is applied to all LEDs that are operated. The simulated thermal resistances from junction to board bottom  $R_{\text{th,j-b,real,CW}}$  and  $R_{\text{th,j-b,real,PCA}}$  are given in Table 4. They have been calculated according to

$$\begin{aligned} & R_{\text{th,j-b,real,CW}} = (T_{j,\text{av,CW}} - T_{b,\text{max}}) / P_{\text{th,total,}} \\ & R_{\text{th,j-b,real,PCA}} = (T_{j,\text{av,PCA}} - T_{b,\text{max}}) / P_{\text{th,total,}} \end{aligned}$$

where the indices CW and PCA denote the operation mode,  $T_{j,av,CW}$  and  $T_{j,av,PCA}$  denote the average junction temperatures of the white and amber LEDs, respectively, and  $P_{th,total}$  the total thermal power. Corresponding thermal resistances  $R_{th,j-b,el,CW}$  and  $R_{th,i-b,el,PCA}$  have been determined using a WPE of 0.30 and 0.25, respectively.

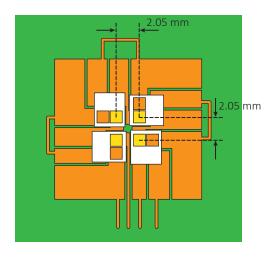


Figure 9. Board geometry with closely spaced LEDs used in the simulations

Table 4. Simulated LED-junction-to-board-bottom thermal resistances for the LED array shown in Figure 9. The thermal resistances  $\mathbf{R}_{\text{th,j-b,el,CW}}$  and  $\mathbf{R}_{\text{th,j-b,el,PCA}}$  have been calculated assuming a WPE of 0.30 and 0.25 for the CW emitter and the PCA emitter, respectively.

	CW		PCA	
BOARD MATERIAL AND DIELECTRIC	R <sub>th,j-b,real</sub> (K/W)	R <sub>th,j-b,el</sub> (K/W)	R <sub>th,j-b,real</sub> (K/W)	R <sub>th,j-b,el</sub> (K/W)
1.0 mm Cu-IMS, 3 W/(mK) - 38 µm dielectric	1.8	1.3	1.8	1.4

#### 4.3 Thermal Measurement Instructions

The use of a temperature probe may be desirable to verify the overall system design model and expected thermal performance. Different methods exist to determine the LED temperature in terms of case temperature ( $T_c$ ), junction temperature  $(T_p)$ , or phosphor temperature  $(T_{oh})$ . Table 5 lists three methods, along with the expected measurement accuracy. The more accurate the measurement is, the closer  $T_c$  and  $T_i$  can be designed to their maximum allowable values as specified in the LUXEON Altilon SMD DT datasheet.

Table 5. Temperature Measurement Methods

METHOD	ACCURACY [°C]	EFFORT	EQUIPMENT COST
Thermo sensor (e.g. thin wire thermocouple)	± 2.0 to ± 5.0 <sup>[1]</sup>	Low	Low
Forward voltage measurement	± 0.5	High	High
Infrared thermal imaging	± 2.0 to ± 10.0 [2]	Medium	High

#### Notes for Table 5:

- 1. See section "Temperature Probing by Thermo Sensor" for parameters determining the measurement accuracy.

  2. See section "Temperature Measurement by IR thermal imaging" for parameters determining the measurement accuracy.

#### **Temperature Probing by Thermo Sensor**

Figure 10 schematically shows the LED soldered to a PCB, including the relevant temperatures as defined for specific positions in the setup. A practical way to verify the case temperature is to measure the temperature  $T_{\text{sensor}}$  on a predefined sensor pad thermally close to the case by means of a thermocouple or a thermistor as shown in Figure 10. The solder mask must be removed to ensure good thermal contact of the thermocouple to the board and to obtain accurate readings. To get a large signal, it is recommended to use the highest possible drive current for the application.

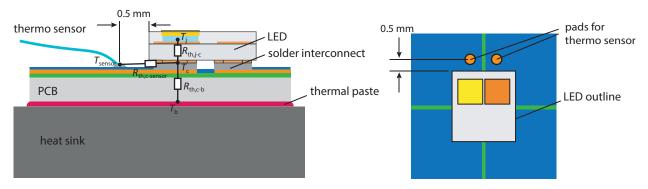


Figure 10. Temperature probing by thermo sensor (schematically) for LUXEON Altilon SMD DT

The case temperature can be calculated according the following equations:

$$T_{c} = T_{\text{sensor}} + R_{\text{th.c-sensor.el}} \cdot P_{\text{el.}}$$

$$T_c = T_{\text{sensor}} + R_{\text{th c-sensor real}} \cdot P_{\text{th}}$$

In these equations,  $T_{\text{sensor}}$  is the sensor temperature at the predefined location and Pel is the electrical power of the LUXEON Altilon DT emitter (CW or PCA),  $P_{\text{th}} = P_{\text{el}} \cdot (1 - \text{WPE})$  is the thermal power of the LUXEON Altilon DT emitter (CW or PCA),  $R_{\text{th,c-sensor,el}}$  is the thermal resistance between case and sensor point based on the electrical power, and  $R_{\text{th,c-sensor,eal}}$  is the thermal resistance between case and sensor point based on the thermal power. The thermal resistances  $R_{\text{th,c-sensor,el}}$  and  $R_{\text{th,c-sensor,eal}}$  are application specific and can be determined with help of thermal simulations and measurements. Lumileds has determined the typical  $R_{\text{th,c-sensor,eal}}$  and  $R_{\text{th,c-sensor,eal}}$  for LUXEON Altilon DT on different board types (see Table 6). The sensor has been mounted at a distance of 0.5 mm from the edge of the package. The accuracy of the measurement depends on the board type, the measurement accuracy of the thermocouple and the mounting position. The temperature signal at the thermocouple measurement point is larger for boards with large heat spreading in the top Cu layer (typically boards with low-conductivity dielectric). LED boards with different configuration, design, or material from the ones given in Table 6 may require additional thermal modeling or measurements to determine the right case-to-sensor thermal resistances.

Table 6. Typical  $R_{th,c\text{-sensor,real}}$  and  $R_{th,c\text{-sensor,el}}$  values of different board concepts. The thermal resistances  $R_{th,c\text{-sensor,el}}$  have been calculated from  $R_{th,c\text{-sensor,real}}$  assuming a WPE of 0.3 for the CW emitter and a WPE of 0.25 for the PCA emitter

	CW		PCA	
BOARD TYPE	R <sub>th,c-sensor,real</sub> (K/W)	R <sub>th,c-sensor,el</sub> (K/W)	R <sub>th,c-sensor,real</sub> (K/W)	R <sub>th,c-sensor,el</sub> (K/W)
Cu-IMS with dielectric of 3 W/(mK) and 38 µm thickness, 35 µm Cu	5.0	3.5	5.0	3.7
FR4 open vias, 35 µm Cu	7.0	4.9	7.0	5.3

#### **Temperature Probing by Forward Voltage Measurement**

The forward voltage measurement uses the temperature dependence of the LED's forward voltage. The forward voltage after switching off the thermally stabilized system is measured and analyzed, yielding information on the LED junction temperature. By using a thermal model of LUXEON Altilon SMD DT or the LED junction-to-case thermal resistances as indicated in the datasheet, the case temperature  $T_c$  can be estimated. To ensure high accuracy, a precise and fast voltage measurement system is needed. In addition, the relationship between forward voltage and temperature needs to be properly characterized for each individual LED. Please contact your sales representatives for further support in this topic.

#### **Temperature Probing by Infrared Thermal Imaging**

Infrared (IR) thermal imaging can be used to measure the surface temperature/phosphor temperature of the LED or the board temperature. Lumileds does not recommend to use IR measurements to estimate the LED junction or case temperature.

For an accurate determination of the absolute temperature via IR thermography, the determination of the exact emissivity value is crucial. The emissivity generally depends on material, surface properties, and temperature. It can be determined by heating up the unbiased device to a defined temperature that can be, for example, measured with a thermocouple. Then, an IR measurement can be taken of this setup, and the emissivity setting of the material of interest (typcially the phosphor or the board surface) can be adjusted to match the thermocouple reading. The obtained emissivity value can be used to evaluate the IR image of the device in operation to determine the temperature of interest. The temperature at which the emissivity value is determined should be similar to the temperature in operation that is to be measured. During IR imaging, make sure that the recorded image is not disturbed by unwanted background reflections. Due to the small dimensions of the LUXEON Altilon SMD DT, an imaging system with high magnification should be used in order to get a sufficient resolution of the LED in the IR image.

Note that due to losses in the phosphor converter layer, the phosphor temperature of the LUXEON Altilon SMD DT is typically higher than the LED junction temperature and that the absolute temperature difference depends on the drive current.

## 5. Assembly Process Guidelines

#### 5.1 Solder Paste

For reflow soldering, a standard lead free SAC solder paste (SnAgCu) with no clean flux can be used. The majority of the Lumileds internal testing has been conducted with the Indium 8.9HF SAC305 solder paste, which showed reasonable reflow and voiding performance for the given settings. An Innolot based solder paste can improve thermal cycling reliability performance under certain conditions. We recommend Heraeus F640IL Innolot in combination with Cu-IMS Boards. Vacuum soldering equipment can be used to achieve a lower void level. Solder paste with powder type 3 is recommended for required stencil thickness and aperture size.

## 5.2 Stencil Design

For solder mask defined land pattern, the appropriate stencil aperture is given in Figure 11. The corner radius of stencil aperture should be selected according to paste particle size to improve paste release. For type 3 paste, a radius of 100  $\mu$ m or larger is recommended.

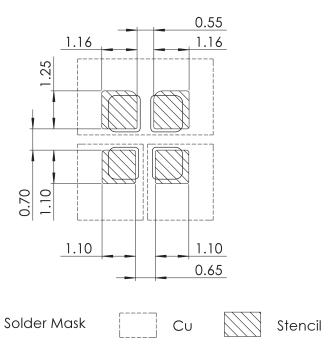


Figure 11. LUXEON Altilon SMD 1x2, 8 mil thick stencil with 115 % aperture, 150 µm bond line thickness

For designs where overprint is used, the solder paste is printed on top of the solder mask. This area should be flat. A trench in the copper layer underneath or close to it should not be used. Otherwise solder paste may be trapped during reflow, leading to solder balling.

#### 5.3 Pick-and-Place

The Nozzle tip geometry should be rectangular. Figure 12 shows a standard pick and place nozzle design for a typical SMT machine vendor, which can be used to handle the LUXEON Altilon SMD DT.

Table 7 shows the standard pick and place nozzle designs, which can be used to handle the LUXEON Altilon SMD DT.

Table 7. Nozzle recommendation for LUXEON Altilon SMD DT

STANDARD NOZZLE (ORDER CODE)	03054923-01
Supplier	ASM Siplace
Nozzle form	Rectangular
Material: Housing / Tip	Vectra A230
Name	2033
Measurements [mm]:	A=2.2x1.6 a=1.7x1.1
Suitable for: LUXEON Altilon SMD DT	

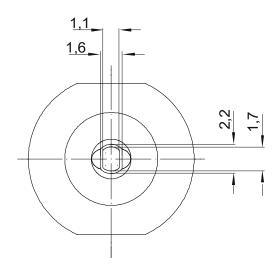


Figure 12. Standard nozzle for SMD DT

### 5.4 Placement Force / Height Control

In order to avoid any damage of the LED and minimize squeeze-out of solder paste, placement process needs to be tightly controlled. Lumileds recommends using low placement forces during the pick and place process. The force should not exceed 2.0 N. (see Figure 13). An additional large dynamic peak force occurs if the LED is placed with high Z-axis velocity at the point of touching on the LED surface, especially if the nozzle mass is high. Under worst case conditions the phosphor LED coating can be damaged. Lower the Z-axis velocity if needed.

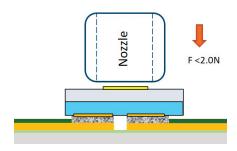


Figure 13. Pick and place force side view

## 5.5 Feed System

Pick and place machines are typically equipped with special pneumatic or electric feeders to advance the tape containing the LEDs. The indexing step in the pick and place process may cause some LEDs to accidentally jump out of the pocket tape or may cause some LEDs to get misaligned inside the pocket tape, resulting in pick-up errors. Depending on the feeder design, minor modifications to the feeder can substantially improve the overall pick and place performance of the machine and reduce/eliminate the likelihood of scratch or damage to the LEDs. An optimum situation will be given when the pickup position is right after cover tape peel off. Do not leave index positions uncovered between peel off and pick position. This will prevent the LEDs from tilting over or jumping out when indexing. Furthermore, the cover tape peeling angle, relative to the tape, should be small to reduce the vertical pulling force during indexing (see Figure 14).

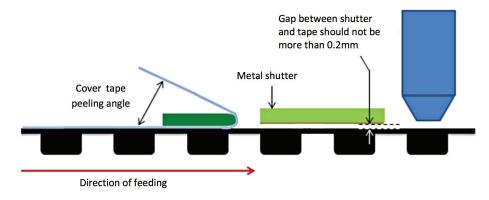


Figure 14. Pick position and cover tape peeling for LUXEON Altilon SMD DT

#### 5.6 Reflow Profile

The LUXEON Altilon SMD DT is compatible with standard surface-mount and lead-free reflow technologies. This greatly simplifies the manufacturing process by eliminating the need for adhesives and epoxies. The reflow step itself is the most critical step in the reflow soldering process and occurs when the boards move through the oven and the solder paste melts, forming the solder joints. To form good solder joints, the time and temperature profile throughout the reflow process must be well maintained.

A temperature profile consists of three primary phases:

- 1. **Preheat:** the board enters the reflow oven and is warmed up to a temperature lower than the melting point of the solder alloy.
- 2. **Reflow:** the board is heated to a peak temperature above the melting point of the solder, but below the temperature that would damage the components or the board.
- 3. Cool down: the board is cooled down rapidly, allowing the solder to freeze, before the board exits the oven.

As a point of reference, the melting temperature for SAC 305 is 217 °C, and the minimum peak reflow temperature is **235 °C.** Lumileds successfully utilized this reflow profile in for LUXEON Altilon SMD DT on FR4 and MCPCB.

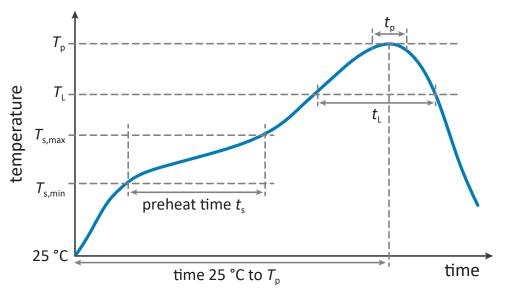


Figure 15. Reflow profile definition according to JEDEC J-STD-020E

Table 8. Temperature measurement methods

PROFILE FEATURE	TYPICAL VALUE	IPC/JEDEC J-STD-020D
Preheat Minimum Temperature ( $\mathcal{T}_{\text{smin}}$ )	150 °C	150 °C
Preheat Maximum Temperature ( $\mathcal{T}_{\text{smax}}$ )	200 °C	200 °C
Preheat Time ( $T_{\rm smin}$ to $T_{\rm smax}$ )	100 s	60 to 120 s
Ramp-Up Rate ( $T_{\rm smax}$ to $T_{\rm p}$ )	2 °C/s average	3 °/s
Liquidus Temperature ( $\mathcal{T}_{\scriptscriptstyle L}$ )	217 °C	217 °C
Time Maintained Above Temperature $\mathcal{T}_{_{\! L}}(t_{_{\! L}})$	60 s	60 to 150 s
Peak / Classification Temperature ( $T_p$ )	240 °C	260 °C
Time Within 5 °C of Actual Peak Temperature ( $t_{\scriptscriptstyle P}$ )	20 s	30 s
Maximum Ramp-Down Rate ( $T_{\rm p}$ to $T_{\rm L}$ )	2.5 °C/second average	6 °C/s
Time 25 °C to Peak Temperature	310 s	480 s
Time Nitrogen Atmosphere (O2)	<1000 ppm	

Note: All temperatures refer to the application Printed Circuit Board (PCB), measured on the surface adjacent to the package body.

Things to watch for after reflow should include:

- 1. Solder voids—perform X-ray inspection
- 2. Solder bridge between anode and cathode
- 3. Solder balling
- 4. Any visible damage, tilt or misplacement of LED
- 5. Any contamination on light emitting area this may impact the light output extraction or cause color shift
- 6. Functional test (open/short)
- 7. Current test, e.g. Vf @ 1 mA  $\geq$  2.0 V

## 5.7 Reflow Accuracy

For solder mask defined designs, Lumileds facilitated internal tests with shown position accuracy after reflow (see Figure 16 and Table 9). Results may vary based on printed circuit board quality and used assembly process. See datasheets for latest information on distances and tolerances.

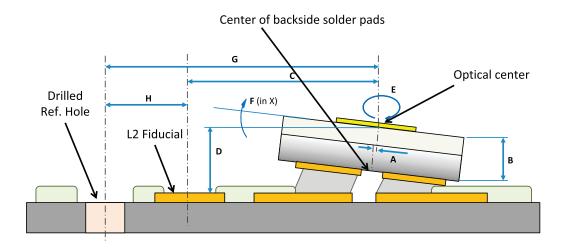


Figure 16. L1 and L2 tolerance definition for LUXEON Altilon SMD DT

Table 9. Dimension and placement tolerances for LUXEON Altilon SMD DT

ITEM	DESCRIPTION	MAXIMUM VALUE	NOMINAL VALUE
A	L1: Optical center to back-side metal x/y	± 50 μm	_
В	L1: Total thickness z	± 50 μm	_
С	L2: Optical center to L2 fiducial, x/y	± 125 μm	± 100 μm
D	L2: Optical center to L2 fiducial, z **	± 105 μm	± 75 μm
Е	L2: Optical center to L2 fiducial, Theta **	± 1.0°	± 0.5°
F	L2: LED package tilting to board **	_	_
G	L2: Optical center to L2 reference hole **	± 105 μm	± 75 μm
Н	L2 Fiducial to L2 reference hole **	± 150 μm	±7 5 μm

Note: \*\* these values depend on EMS supplier capabilities and PCB quality level.

There are ways to improve position accuracy by applying glue locking or select only PCB suppliers that are capable of delivering the required level of quality.

## 5.8 Board Handling and Bending

The LED package handling precaution, as described in section 5.3 and 5.4., must also be applied when handling completed boards. Even though this product has a small form factor and is unlikely to cause any problems, forces on the package should be kept to a minimum. Bending of a PCB is a common handling problem typically seen on large boards. A printed circuit board may warp after reflow when layers with different CTE (coefficient of thermal expansion) are applied to the top and bottom of the boards. If the PCB is subsequently secured to a flat surface, a vertical force is applied to the LED package (see Figure 17).

Any deformation by mounting the board and screwing it onto a heatsink or by de-paneling, like punching-off or breaking-off, should be kept to a minimum. As a general guideline, it should be at most 2 mm of vertical deflection for every 90 mm of FR4 PCB length. The guideline should be maintained to prevent the sapphire chip, used in the LED, from cracking and causing device failure. Reference AEC-Q200-005 for board bending test preparation.

This guideline does not apply to solder joint reliability, as the ability of the solder joint to withstand this stress (elongation) depends on the footprint layout, solder joint thickness, solder voiding and the type of solder paste used.

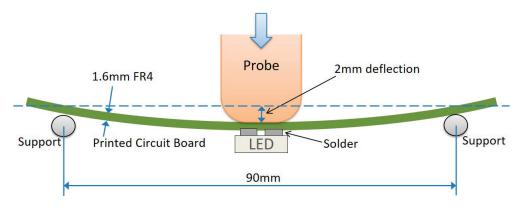


Figure 17. Maximum PCB bending guideline to prevent damage to the LUXEON Altilon SMD DT package

## 6. Interconnect Reliability

The reliability of board interconnect under thermal cycling and thermal shock condition is mainly determined by thermal expansion of used materials. The LUXEON Altilon SMD DT package is made of an AIN which has a low CTE (coefficient of thermal expansion) of ~4 ppm (coefficient of thermal expansion). The CTE mismatch between LED package and printed circuit board will lead to mechanical stress and cause solder fatigue or solder cracking. To achieve highest possible reliability, the CTE of the board material should be as similar to the LED package as possible. Table 10 shows commonly used materials and their CTE.

Table 10. CTE of common board subst	rate materials for LUXEON Altilon SMD DT
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MATERIAL	COEFFICIENT OF THERMAL EXPANSION (CTE)
Sapphire (LED chip)	5-6 ppm
Solder SAC305	19-22 ppm
Copper	16.5 ppm
FR4	12-17 ppm*
Aluminium	23.1 ppm
AlN	4 ppm
$Al_2O_3$	6-8 ppm

<sup>\*</sup> Depending on laminate vendor, prepreg type and fiber orientation.

Also, the mechanical properties of solder material and solder thickness have an impact on interconnect reliability. Using a ductile material and increasing the bond line thickness will increase solder joint reliability.

Table 10 and Table 11 shows what Lumileds testing confirmed and recommends. There are other possible options and customers shall confirm suitability in their application.

Table 11. Thermal cycling performance using different board types, solder material and process for LUXEON Altilon SMD DT

BOARD MATERIAL [1]	BOND LINE THICKNESS	SOLDER MATERIAL	SOLDER PROCESS	THERMAL CYCLING PERFORMANCE [2]
Cu-IMS	150 µm	Innolot	Vacuum Reflow	1000 cycles
FR4 with F&C vias	150 μm	SAC 305	Standard Reflow	1000 cycles

## 7. JEDEC Moisture Sensitivity Level

The LUXEON Altilon SMD has a JEDEC moisture sensitivity level of 1. This is the highest level offered in the industry and the highest level within the JEDEC J-STD-020D.1 standard. This provides the customer with ease of assembly; the customer no longer needs to be concerned about bake out times and floor life. No bake out time is required for a moisture sensitivity level of 1.

Moisture sensitivity level 1 allows the device to be reflowed three times under the specifications as described in the respective LUXEON Altilon Intense datasheets. JEDEC has defined eight levels for moisture sensitivity, as shown in Table 12.

Table 12. JEDEC moisture sensitivity levels for LUXEON Altilon SMD DT

LEVEL	FLOOR LIFE		SOAK REQUIREMENTS			
			STANDARD		ACCELERATED EQUIVALENT 1	
	TIME	CONDITIONS	TIME	CONDITIONS	TIME	CONDITIONS
1	Unlimited	≤30 °C/85 % RH	168 Hours +5/-0	85 °C/85 % RH		
2	1 Year	≤30 °C/60 % RH	168 Hours +5/-0	85 °C/60 % RH		
2a	4 Weeks	≤30 °C/60 % RH	696 Hours +5/-0	30 °C/60 % RH	120 Hours +1/-0	60 °C/60 % RH
3	168 Hours	≤30 °C/60 % RH	192 Hours +5/-0	30 °C/60 % RH	40 Hours +1/-0	60 °C/60 % RH
4	72 Hours	≤30 °C/60 % RH	96 Hours +2/-0	30 °C/60 % RH	20 Hours +5/-0	60 °C/60 % RH
5	48 Hours	≤30 °C/60 % RH	72 Hours +2/-0	30 °C/60 % RH	15 Hours +5/-0	60 °C/60 % RH
5a	24 Hours	≤30 °C/60 % RH	48 Hours +2/-0	30 °C/60 % RH	10 Hours +5/-0	60 °C/60 % RH
6	Time on Label (TOL)	≤30 °C/60 % RH	TOL	30 °C/60 % RH		

<sup>1.</sup> IMS dielectric layer considered as hard dielectric material.
2. Thermal cycling performance is related to a passive test according JEDEC standard J-ESD22-A104E: Condition G -40/+125°C, 10s transition, 30min dwell.

## 8. Packaging Considerations—Chemical Compatibility

The LUXEON Altilon SMD DT package contains a silicone overcoat to protect the LED chips and extract the maximum amount of light. As with most silicones used in LED optics, care must be taken to prevent any incompatible chemicals from directly or indirectly reacting with the silicone.

The silicone overcoat in LUXEON Altilon SMD DT is gas permeable. Consequently, oxygen and volatile organic compound (VOC) gas molecules can diffuse into the silicone overcoat. VOCs may originate from adhesives, solder fluxes, conformal coating materials, potting materials and even some of the inks that are used to print the PCBs. Some VOCs and chemicals react with silicone and produce discoloration and surface damage. Other VOCs do not chemically react with the silicone material directly but diffuse into the silicone and oxidize during the presence of heat or light. Regardless of the physical mechanism, both cases may affect the total LED light output. Since silicone permeability increases with temperature, more VOCs may diffuse into and/or evaporate out from the silicone.

Careful consideration must be given to whether LUXEON Altilon SMD DT emitters are enclosed in an "air tight" environment or not. In an "air tight" environment, some VOCs that were introduced during assembly may permeate and remain in the silicone overcoat. Under heat and "blue" light, the VOCs inside the silicone overcoat may partially oxidize and create a silicone discoloration, particularly on the surface of the LED where the flux energy is the highest. In an air rich or "open" air environment, VOCs have a chance to leave the area (driven by the normal air flow). Transferring the devices, which were discolored in the enclosed environment back to "open" air, may allow the oxidized VOCs to diffuse out of the silicone overcoat and may restore the original optical properties of the LED.

Determining suitable threshold limits for the presence of VOCs is very difficult since these limits depend on the type of enclosure used to house the LEDs and the operating temperatures. Also, some VOCs can photo-degrade over time.

Table 13 provides a list of commonly used chemicals that should be avoided as they may react with the silicone material. Note that Lumileds does not warrant that this list is exhaustive since it is impossible to determine all chemicals that may affect LED performance.

The chemicals in Table 13 are typically not directly used in the final products that are built around LUXEON Altilon SMD DT LEDs. However, some of these chemicals may be used in intermediate manufacturing steps (e.g. cleaning agents). Consequently, trace amounts of these chemicals may remain on sub-components, such as heatsinks. Lumileds, therefore, recommends the following precautions when designing your application:

- 1. When designing secondary lenses to be used over an LED, provide a sufficiently large air-pocket and allow for "ventilation" of this air away from the immediate vicinity of the LED.
- 2. Use mechanical means of attaching lenses and circuit boards as much as possible. When using adhesives, potting compounds and coatings, carefully analyze its material composition and do thorough testing of the entire fixture under High Temperature Over Life (HTOL) conditions.

Table 13. List of commonly used chemicals that may damage the silicone encapsulant of LUXEON Altilon SMD DT

CUENICAL NAME	TVDICALUCE		
CHEMICAL NAME	TYPICAL USE		
Hydrochloric Acid	Acid		
Sulfuric Acid	Acid		
Nitric Acid	Acid		
Acetic Acid	Acid		
Sodium Hydroxide	Alkali		
Potassium Hydroxide	Alkali		
Ammonia	Alkali		
MEK (Methyl Ethyl Ketone)	Solvent		
MIBK (Methyl Isobutyl Ketone)	Solvent		
Toluene	Solvent		
Xylene	Solvent		
Benzene	Solvent		
Gasoline	Solvent		
Mineral spirits	Solvent		
Dichloromethane	Solvent		
Tetrachloromethane	Solvent		
Castor Oil	Oil		
Lard	Oil		
Linseed Oil	Oil		
Petroleum	Oil		
Silicone Oil	Oil		
Halogenated Hydrocarbons (containing F, Cl, Br elements)	Misc.		
Rosin Flux	Solder Flux		
Acrylic Tape	Adhesive		



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